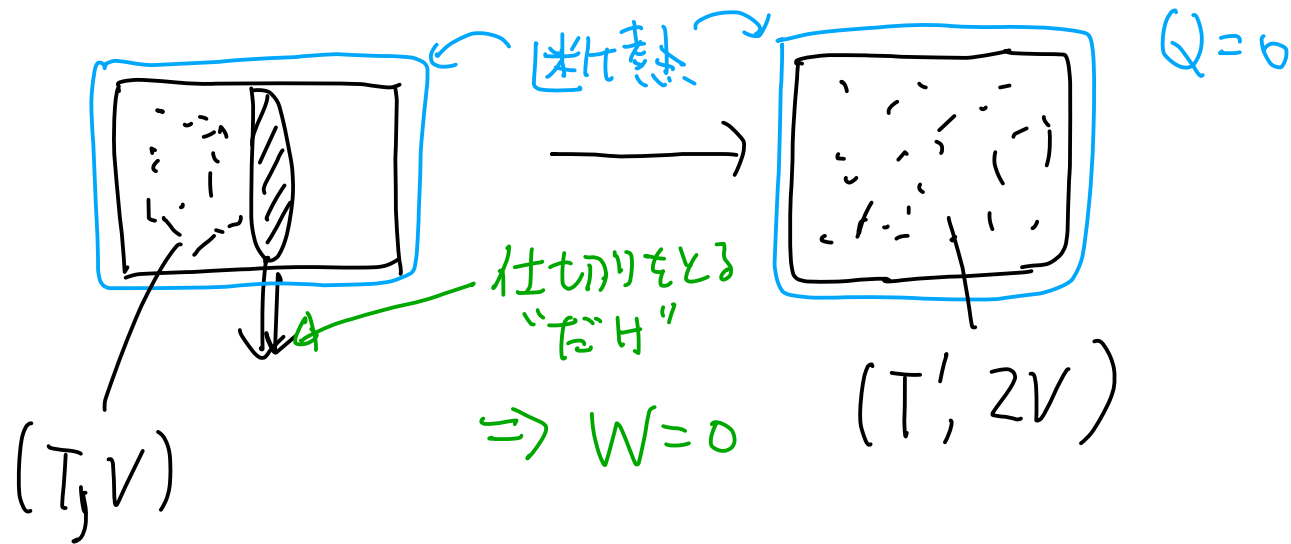


熱力学講義 XII

20/07/29

§ 断熱自由膨張



- $U(T', 2V) - U(T, V) = 0$

- $S(T', 2V) - S(T, V) \geq 0$

§ 151: ファンデルワールス気体

$$\checkmark \quad P(T, V) = \frac{NRT}{V - Nb} - a\left(\frac{N}{V}\right)^2 \quad (a > 0) \quad (b > 0; V > Nb)$$

$$\Rightarrow F(T, V) - F(T, V_0) = - \int_{V_0}^V dV' P(T, V')$$

$$= -NRT \log \frac{V - Nb}{V_0 - Nb} - aN \left(\frac{N}{V} - \frac{N}{V_0} \right)$$

$$\Rightarrow S(T, V) - S(T, V_0) = +NR \log \frac{V - Nb}{V_0 - Nb}$$

$$\leftarrow dF = -SdT - PdV$$

$$U(T, V) - U(T, V_0) = -aN \left(\frac{N}{V} - \frac{N}{V_0} \right)$$

$$\leftarrow F = U - TS$$

§ 例: ファンデルワールス気体 II

$$C(T, V) = \frac{3}{2} NR$$

$$U(T, V) - U(T_0, V) = \frac{3}{2} NR(T - T_0)$$

$$S(T, V) - S(T_0, V) = \frac{3}{2} NR \log \frac{T}{T_0}$$

$$C = \left(\frac{\partial U}{\partial T} \right)_V$$

$$= T \left(\frac{\partial S}{\partial T} \right)_V$$

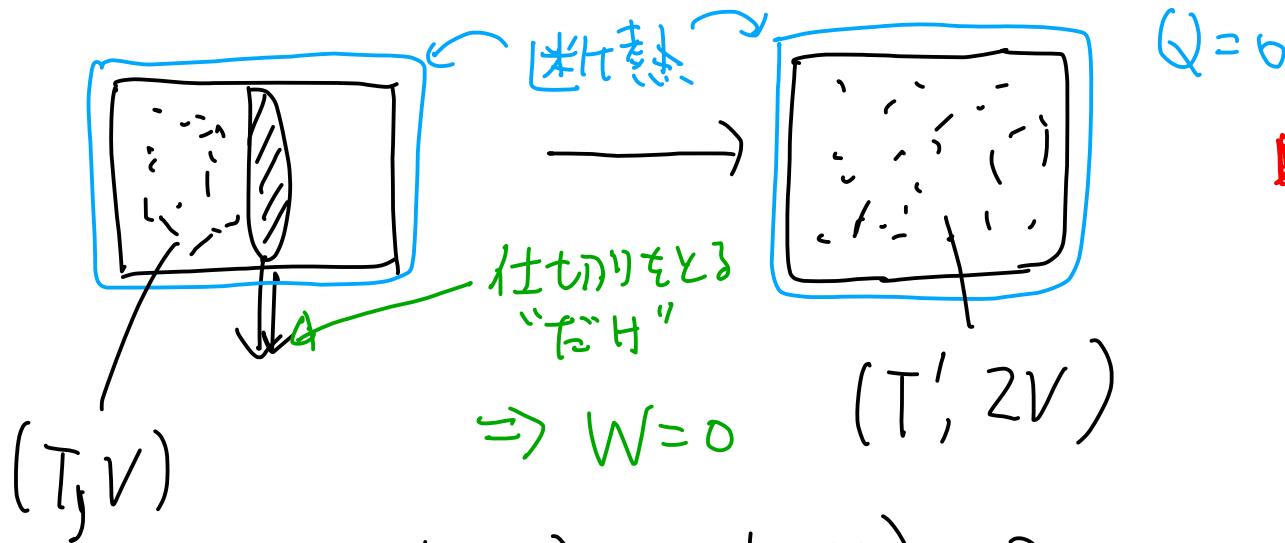
$$\therefore \left\{ \begin{array}{l} U(T, V) = \frac{3}{2} NR T - a \left(\frac{N^2}{V} \right) + \text{const} \end{array} \right.$$

$$S(T, V) = \frac{3}{2} NR \log T + NR \log \frac{V - Nb}{N}$$

$$F(T, V) = \frac{3}{2} NR T - a \left(\frac{N^2}{V} \right) - T NR \log \frac{T^{3/2} (V - Nb)}{N} + \text{const}$$

§ 溫度變化

斷熱自由膨脹



$T' < T$
物理的描像

$T' > 0$ 对

$$T > \frac{aN}{3RV}$$

一般に

$$T > \frac{2aN}{3RV}$$

$$U(T', 2V) - U(T, V) = 0$$

$$\Leftrightarrow \frac{3}{2}NR(T' - T) - aN^2\left(\frac{1}{2V} - \frac{1}{V}\right) = 0$$

$$T' - T = -\frac{aN}{3RV} < 0$$

§ エントロピー変化

$$S(T, V) = \frac{3}{2}NR \log T + NR \log \frac{V - Nb}{N}$$

$$S(T', 2V) - S(T, V) = \frac{3}{2}NR \log \frac{T'}{T} + NR \log \frac{2V - Nb}{V - Nb}$$

$$= \underbrace{\frac{3}{2}NR \log \left(1 - \frac{aN}{3RV T}\right)}_{\text{負}} + \underbrace{NR \log \frac{2V - Nb}{V - Nb}}_{\text{正}}$$

$S(T', 2V) - S(T, V) > 0$ のはず"だから"---?

~ Intermission ~

§ 安定性の条件

$$\left(\frac{\partial P}{\partial V}\right)_T \leq 0 \quad \Rightarrow \quad \frac{\partial^2 \bar{F}(T, V)}{\partial V^2} \geq 0$$

$$F(T, V) = \frac{3}{2} NRT - a\left(\frac{N^2}{V}\right) - TNR \log \frac{T^{3/2}(V-Nb)}{N} + \text{const}$$

$$\Rightarrow -2a \frac{N^2}{V^3} + TNR \frac{1}{(V-Nb)^2} \geq 0 \quad 2 \frac{aN^2}{RTV^3} \leq \frac{1}{(V-Nb)^2}$$

$$\frac{aN}{3RTV^2} = \frac{aN V^2}{3RTV^3}$$

$$\leq \frac{1}{6} \frac{V^2}{(V-Nb)^2} \quad //$$

§ I → 0°C - 変化

$$\Delta S \equiv S(T', 2V) - S(T, V)$$

$$= \frac{3}{2}NR \log \left(1 - \frac{a^2 N}{3RV^2} \right) + NR \log \frac{2V - Nb}{V - Nb}$$

$$\frac{36}{216}$$

$$> \frac{3}{2}NR \log \left(1 - \frac{1}{6} \frac{V^2}{(V - Nb)^2} \right) + NR \log \frac{2V - Nb}{V - Nb}$$

b=0

$$= \frac{3}{2}NR \log \frac{5}{6} + NR \log 2$$

$$= \frac{3}{2}NR \left(\log \frac{5}{6} + \log 2^{2/3} \right)$$

$$> 0$$

$$2^{2/3} \cdot \frac{5}{6} > 1$$

$$\Leftrightarrow 4 \cdot \left(\frac{5}{6}\right)^3 > 1$$

$$\Leftrightarrow \frac{4 \times 125}{216} > 1$$

$$4 \left(\frac{2}{3}\right)^3 = \frac{32}{27}$$

§ I → 0°C - 変化 (一般)

$$\Delta S \equiv S(T', 2V) - S(T, V)$$

$$= \frac{3}{2}NR \log \left(1 - \frac{aN}{3RV T} \right) + NR \log \frac{2V - Nb}{V - Nb}$$

$$\frac{3b}{2V}$$

$$\geq \underbrace{\frac{3}{2}NR \log \left(1 - \frac{1}{6} \frac{V^2}{(V - Nb)^2} \right)}_{\text{負の大きい数にたよる?}} + NR \log \frac{2V - Nb}{V - Nb}$$

b > 0
?

負の大きい数にたよる?

$\Delta S > 0$ 証明可能か? ... ??

§ エントロピー変化 (系統)

$$\begin{aligned}\Delta S &\equiv S(T', 2V) - S(T, V) \\ &= \frac{3}{2}NR \log\left(1 - \frac{aN}{3RV T}\right) + NR \log \frac{2V - Nb}{V - Nb}\end{aligned}$$

$$\frac{aN}{3RV T} < \frac{1}{2}, \quad 2V - Nb > 2V - 2Nb$$

$$\begin{aligned}\Rightarrow \Delta S &> \frac{3}{2}NR \log \frac{1}{2} + NR \log 2 \\ &= \frac{3}{2}NR \log\left(\frac{1}{2}\right) \cdot 2^{\frac{2}{3}} \\ &= \frac{1}{2}NR \log \frac{2^2}{2^3} > 0\end{aligned}$$

§ イントロ-変化 (系壳)

$$\begin{aligned}\Delta S &\equiv S(T', 2V) - S(T, V) \\ &= \frac{3}{2}NR \log \left(1 - \frac{a^N}{3RV T}\right) + NR \log \frac{2V - Nb}{V - Nb} \\ &= \frac{3}{2}NR \log \left(1 - \frac{aP}{3RT}\right) + NR \log \left(\frac{2 - bp}{1 - bp}\right) \\ &\approx NR \Psi(P)\end{aligned}$$

$$\Psi(P) \equiv \frac{3}{2} \log \left(1 - \frac{aP}{3RT}\right) + \log \left(\frac{2 - bp}{1 - bp}\right)$$

$$\begin{cases} aP(1 - Pb) \leq TR & (\text{圧力正}) \\ 2aP(1 - bp)^2 \leq TR & (\text{安定性}) \end{cases}$$

§ 計算

$$\Psi(p) = \frac{3}{2} \log \left(1 - \frac{ap}{3RT} \right) + \log \left(\frac{2-bp}{1-bp} \right)$$

$$\begin{cases} ap(1-bp) \leq TR & (\text{正}) \\ 2ap(1-bp)^2 \leq TR & (\text{安定性}) \end{cases} \Rightarrow \frac{1}{2}ap \leq TR$$

$$\Psi'(p) = \underbrace{\frac{3}{2} \frac{(-1)}{1 - \frac{ap}{3RT}} \frac{a}{3RT}}_{\text{負}} + \underbrace{\frac{-b}{2-bp} + \frac{b}{1-bp}}_{\text{正}}$$

... 0 0 0 ...

~ Intermission ~

§ 考え方の転換

$$U(T, V) = \frac{3}{2}NR T - a\left(\frac{N^2}{V}\right) + \text{const}$$

$$S(T, V) = \frac{3}{2}NR \log T + NR \log \frac{V - Nb}{N}$$

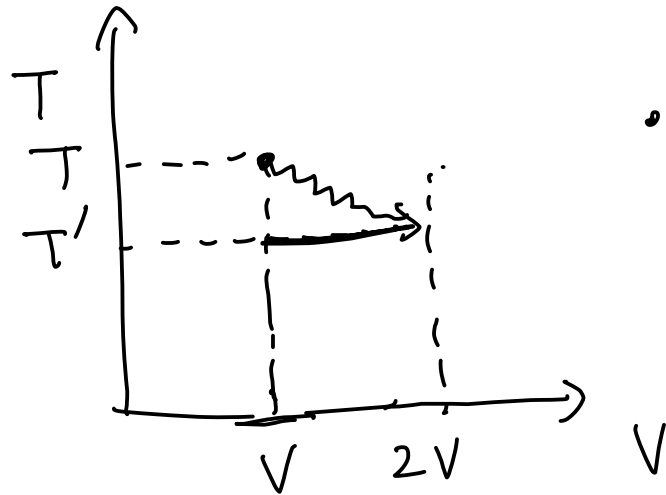
$$\Rightarrow S(U, V) = \frac{3}{2}NR \log \left(\frac{U + a\frac{N^2}{V}}{N} \right) + NR \log \frac{V - Nb}{N}$$

$$\Delta S = S(T', 2V) - S(T, V)$$

$$= S(U, 2V) - S(U, V)$$

$$= \int_V^{2V} dV' \left(\frac{\partial S}{\partial V'} \right)_U = \int_V^{2V} dV' \frac{P(T(U, V'), V')}{T(U, V')} > 0$$

§ 一般論



$$\bullet U(T', 2V) - U(T, V) = 0$$

$(T', 2V) \xrightarrow{a} (T, V)$ が実現可能 とする

$$\Rightarrow (T', 2V) \xrightarrow{a} (T, V) \xrightarrow{i} (T', V) \xrightarrow{g} (T', 2V)$$

$$Q = U(T', V) - U(T, V) + U(T', 2V) - U(T', V) + \int_V^{2V} P(T', V'') dV''$$

$$= \int_V^{2V} P(T', V'') dV'' > 0$$

第2項は永久機関P

§ 安定性 ?

$$\Delta S = S(T', 2V) - S(T, V)$$

$$= S(U, 2V) - S(U, V)$$

$$= \int_V^{2V} dV' \left(\frac{\partial S}{\partial V'} \right)_U$$

$$= \int_V^{2V} dV' \frac{P}{T} > 0 \quad (\text{圧力の正値性})$$

