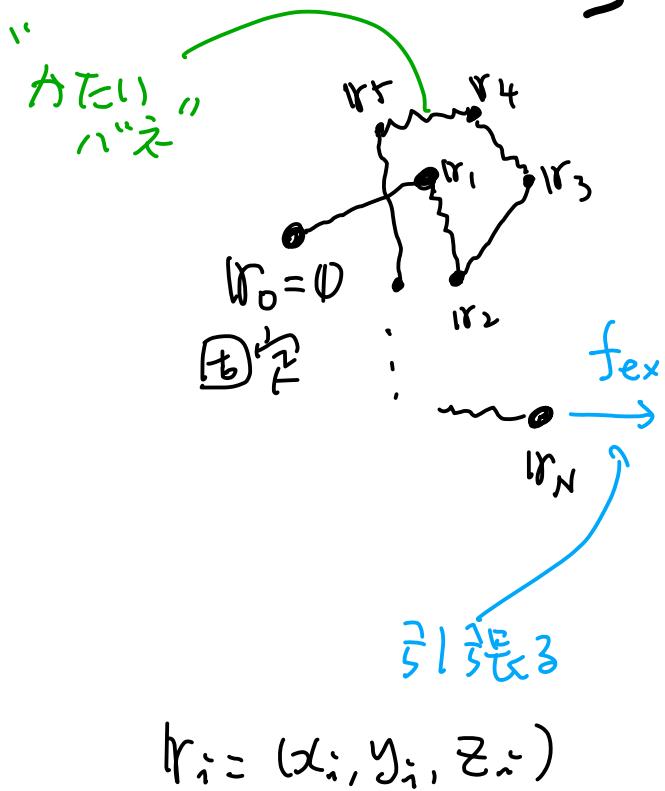


統計力学 A IX

2020/12/08

# § 設定



$$\Gamma = (r_1, r_2, \dots, r_N, p_1, \dots, p_N)$$

$$H(\Gamma; f_{\text{ex}}, N)$$

$$= \sum_{i=1}^N \frac{|p_i|^2}{2m} + \sum_{i=1}^N \frac{K}{2} (|r_i - r_{i-1}| - a)^2 - f_{\text{ex}} x_N$$

- $\beta K a^2 \gg 1$  ;  $\beta = \frac{1}{k_B T}$

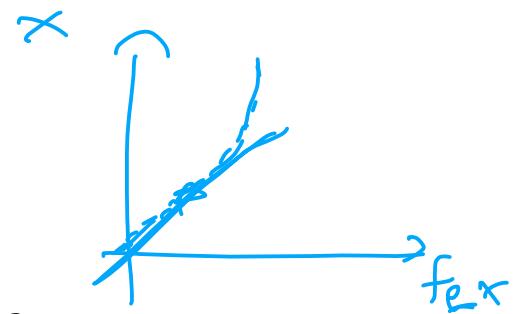
$$X \equiv \langle x_N \rangle_{\beta, f_{\text{ex}}}^c = \int d\Gamma x_N f_{\beta, f_{\text{ex}}}^c(\Gamma)$$

$$f_{\beta, f_{\text{ex}}}^c(\Gamma) \equiv \frac{1}{Z(\beta, f_{\text{ex}}, N)} e^{-\beta H(\Gamma; f_{\text{ex}}, N)}$$

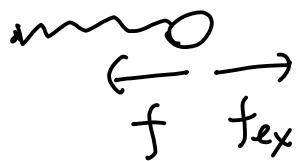
## § 計算すべきこと

$$X = \frac{1}{k_{macro}} f_{ex} + o(f_{ex} \beta a)$$

マクロ  $f_x$  バス定数  $k_{macro}$  を求めよ。



cf: 復元力  $f = -k_{macro}X$   
 $(f + f_{ex} = 0)$



結果  $k_{macro} = k_1 T$  !!

→ 采道！

~Intermission~

§ 例題 - 球殼問題 — 西己道 (= focus —

$$\langle x \rangle = \int dP \frac{x_N}{Z(\beta, f_{ex}, N)} e^{-\beta \left[ \sum_{i=1}^N \frac{|p_i|^2}{2m} + \frac{K}{2} \sum_i (|r_i - r_{i-1}| - a)^2 - f_{ex} x_N \right]}$$

$$= \frac{\int dr_1 \dots dr_N x_N e^{-\beta \left[ \frac{K}{2} \sum_i (|r_i - r_{i-1}| - a)^2 - f_{ex} x_N \right]}}{\int dr_1 \dots dr_N e^{-\beta \left[ \frac{K}{2} \sum_i (|r_i - r_{i-1}| - a)^2 - f_{ex} x_N \right]}}$$

$$Z(\beta, f_{ex}, N) = \int dp_1 \dots dp_N e^{-\beta \sum_{i=1}^{N-1} |p_i|^2} \times \int dr_1 \dots dr_N e^{-\beta \sum_i (|r_i - r_{i-1}| - a)^2 - f_{ex} x_N}$$

$$\text{分子と分母の } \frac{\partial}{\partial f_{ex}} \text{ で消す。} \quad K_B T \frac{\partial}{\partial f_{ex}} Z_c(\beta, f_{ex}, N)$$

## § 第2段階 — 公式 —

$$X = k_B T \frac{\frac{\partial}{\partial f_{ex}} Z_c(\beta, f_{ex}, N)}{Z_c(\beta, f_{ex}, N)}$$

$$= k_B T \frac{\partial}{\partial f_{ex}} \log Z_c(\beta, f_{ex}, N)$$

公式I

$$\therefore Z_c(\beta, f_{ex}, N) = \int d\mathbf{r}_1 \dots d\mathbf{r}_N e^{-\beta \left[ \sum_{i=2}^K (|r_i - r_{i-1}| - a)^2 - f_{ex} x_N \right]}$$

を計算すればよい。

# § 第3段階 - 变数变换 -

$$\begin{aligned}
 Z_c(\beta, f_{ex}, N) &= \int d\mathbf{r}_1 \cdots d\mathbf{r}_N e^{-\beta \left[ \sum_{i=2}^N \frac{k}{2} ((\mathbf{r}_i - \mathbf{r}_{i-1}) - a)^2 - f_{ex} x_N \right]} \\
 &= \int d\mathbf{q}_1 \cdots d\mathbf{q}_N e^{-\beta \sum_{i=1}^N \frac{k}{2} ((\mathbf{q}_i - a)^2 + \beta f_{ex} \xi_i)} \\
 &= \left[ \left\{ d\mathbf{q}_i e^{-\beta \frac{k}{2} ((\mathbf{q}_i - a)^2 + \beta f_{ex} \xi_i)} \right\} \right]^N \\
 &= [Z_c^{(1)}(\beta, f_{ex})]^N
 \end{aligned}$$

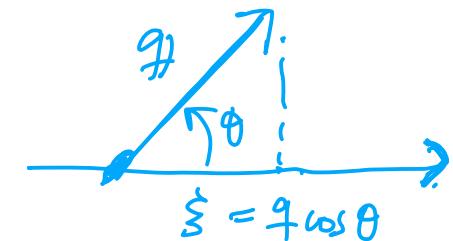
$\mathbf{r}_0 = 0$   
 $\left\{ \begin{array}{l} \mathbf{q}_1 = \mathbf{r}_1 - \mathbf{r}_0 \\ \mathbf{q}_2 = \mathbf{r}_2 - \mathbf{r}_1 \\ \vdots \\ \mathbf{q}_N = \mathbf{r}_N - \mathbf{r}_{N-1} \end{array} \right.$   
 $\mathbf{q}_i = (\xi_i, \eta_i, \zeta_i)$   
 $x_N = \sum_{i=1}^N \xi_i$   
 $e^{x+y} = e^x \cdot e^y$

$$Z_c^{(1)}(\beta, f_{ex}) = \int d\mathbf{q} e^{-\beta \frac{k}{2} ((\mathbf{q} - a)^2 + \beta f_{ex} \xi)}$$

Σ 計算すればよい。

# § 第4段階 - 積分 -

$$Z_C^{(1)}(\beta, f_{\text{ex}}) = \int d\mathbf{q} e^{-\beta \frac{k}{2}(q_x^2 + q_y^2) + \beta f_{\text{ex}} q_z}$$



$$= 2\pi \int_0^\infty dq q^2 e^{-\beta \frac{k}{2}(q-a)^2} \int_0^\pi d\theta \sin\theta e^{\beta f_{\text{ex}} q \cos\theta}$$

$$d\mathbf{q} = 2\pi q^2 \sin\theta dq d\theta$$

$$\therefore Z_C^{(1)}(\beta, f_{\text{ex}}) = \frac{4\pi}{\beta f_{\text{ex}}} \int_0^\infty dq q e^{-\beta \frac{k}{2}(q-a)^2} \sinh(\beta f_{\text{ex}} q)$$

$\downarrow$   
 $t = \cos\theta$   
 $dt = -\sin\theta d\theta$

$$= \frac{1}{\beta f_{\text{ex}} q} \left( e^{\beta f_{\text{ex}} q} - e^{-\beta f_{\text{ex}} q} \right)$$

$$= \frac{2}{\beta f_{\text{ex}} q} \cdot \sinh(\beta f_{\text{ex}} q)$$

# § 第5段階 - 減近形 -

$$\therefore Z_C^{(1)}(\beta, f_{ex}) = \frac{4\pi}{\beta f_{ex}} \int_0^\infty dq q e^{-\beta \frac{k}{2}(q-a)^2} \sinh(\beta f_{ex} q) \quad (\beta k a^2 \gg 1)$$

かたいいばね

$$q = a + \tilde{q}a$$

$$= \frac{4\pi a^2}{\beta f_{ex}} \int_{-1}^{\infty} d\tilde{q} \left(1 + \frac{\tilde{q}}{a}\right) e^{-\beta \frac{k}{2} a^2 \tilde{q}^2} \sinh(\beta f_{ex} (a + \tilde{q}a))$$

$$= \frac{4\pi a^2}{\beta f_{ex}} \left[ \sinh \beta f_{ex} a \int_{-\infty}^{\infty} d\tilde{q} e^{-\beta \frac{k}{2} a^2 \tilde{q}^2} + O\left(\frac{1}{\beta k a^2}\right) \right]$$

主要項は zero

$$= \frac{4\pi a^2}{\beta f_{ex}} \sinh \beta f_{ex} a \sqrt{\frac{2\pi}{\beta k a^2}}$$

主な貢献

# § 第6段階 - 総束形化 -

$$X = k_B T N \frac{\partial}{\partial f_{ex}} \log Z_C^{(c)}(\beta, f_{ex})$$

$$= k_B T N \frac{\partial}{\partial f_{ex}} \left[ \log (\sinh \beta f_{ex} a) - \log f_{ex} \right]$$

$$= k_B T N \left[ \frac{\cosh(\beta f_{ex} a)}{\sinh(\beta f_{ex} a)} \beta a - \frac{1}{f_{ex}} \right]$$

$\cosh(\beta f_{ex} a)$   
 $\sinh(\beta f_{ex} a)$   
 $\beta a$   
 $1 + \frac{1}{2}(\beta f_{ex} a)^2 + \dots$   
 $\beta f_{ex} a + \frac{1}{6}(\beta f_{ex} a)^3 + \dots$

$$= \frac{1}{f_{ex}} \frac{1 + \frac{1}{2}(\beta f_{ex} a)^2 + \dots}{1 + \frac{1}{6}(\beta f_{ex} a)^2 + \dots} = \frac{1}{f_{ex}} \left( 1 + \frac{1}{3}(\beta f_{ex} a)^2 + \dots \right)$$

$$\begin{aligned} \therefore X &= k_B T N \frac{1}{3} \beta^2 a^2 f_{ex} + o((\beta f_{ex} a)) \cdot aN \\ &= N \frac{a^2}{3 k_B T} f_{ex} + o((\beta f_{ex} a)) \cdot aN \end{aligned}$$

# § 計算のまとめ

$$X = N \frac{a^3}{3 k_B T} f_{ex}$$

$$= N_a \cdot \frac{a f_{ex}}{3 k_B T} q$$

熱膨張係数と  
外からのすす仕事

$$= \frac{1}{k_{macro}} f_{ex}$$

(自由度あたりの  
運動エネルギー)

$$k_{macro} = \frac{3 k_B T}{N a^2}$$

復元力  
 $f = - k_{macro} X$

マクロなバネ定数が  
あらわした !!

~Intermission~

# § 分子力関数

$$\begin{aligned}
 Z(\beta, f_{\text{ex}}, N) &= \int dP e^{-\beta \left[ \sum_i \frac{(p_i)^2}{2m} + \sum_i^K \frac{1}{2} ((r_i - r_{i-1}) - a)^2 - \beta f_{\text{ex}} x_N \right]} \\
 &= \left( \int dp e^{-\beta \frac{p^2}{2m}} \right)^{3N} \cdot \left( \frac{4\pi a^2}{\beta f_{\text{ex}}} \sinh \beta f_{\text{ex}} a \sqrt{\frac{2\pi}{\beta K a^2}} \right)^N \\
 &= \left( \frac{2m\pi}{\beta} \right)^{\frac{3N}{2}} \left( \frac{\sinh \beta f_{\text{ex}} a}{\beta f_{\text{ex}} a} \right)^N (4\pi a^3)^N \left( \frac{2\pi}{\beta K a^2} \right)^{\frac{N}{2}}
 \end{aligned}$$

$$\log Z(\beta, f_{\text{ex}}, N) = -2N \log \beta + N \log \underbrace{\frac{\sinh(\beta f_{\text{ex}} a)}{\beta f_{\text{ex}} a}}_{\text{定数}} + N C_0$$

$\sim \log \left( 1 + \frac{1}{6} (\beta f_{\text{ex}} a)^2 + \dots \right) = \frac{1}{6} (\beta f_{\text{ex}} a)^2 = \frac{1}{2} \beta \cancel{\frac{1}{N}} f_{\text{ex}}$

$$X = N \frac{a^3}{3k_B T} f_{\text{ex}}$$

# § I. 乃ルギー

$$\log Z(\beta, f_{\text{ex}}, N) = -2N \log \beta + N \log \frac{\sinh(\beta f_{\text{ex}}a)}{\beta f_{\text{ex}}a} + N C_0$$

$$\langle H \rangle_{\beta, f_{\text{ex}}, N} = \frac{1}{Z(\beta, f_{\text{ex}}, N)} \int dP H(P; f_{\text{ex}}, N) e^{-\beta H(P; f_{\text{ex}}, N)}$$

$$= - \frac{\partial}{\partial \beta} \log Z(\beta, f_{\text{ex}}, N)$$

$$= 2N k_B T + N k_B T - N \frac{\cosh(\beta f_{\text{ex}}a)}{\sinh(\beta f_{\text{ex}}a)} f_{\text{ex}}a$$

$$= 3N k_B T - \frac{N}{\beta a f_{\text{ex}}} \left( 1 + \frac{1}{3} (\beta f_{\text{ex}}a)^2 + \dots \right) f_{\text{ex}}a$$

$$= 2N k_B T - \frac{N}{3} (\beta f_{\text{ex}}a)^2 k_B T$$

$$= 2N k_B T - X \cdot f_{\text{ex}}$$

$$X = N \frac{a^2}{3 k_B T} f_{\text{ex}}$$

//

# § イントロビー - 公式 -

$$\begin{aligned} Z(\beta, f_{\text{ex}}, N) &= \int dP e^{-\beta H(P; f_{\text{ex}}, N)} \\ &= \int dP \underbrace{\int dE \delta(E - H(P; f_{\text{ex}}, N))}_{\rightarrow = 1} e^{-\beta H(P; f_{\text{ex}}, N)} \\ &= \int dE e^{-\beta E} \sum(E, f_{\text{ex}}, N) \end{aligned}$$

$$\sum(E, f_{\text{ex}}, N) = \int dP \delta(E - H(P; f_{\text{ex}}, N))$$

(N! うまい)

$$= e^{\frac{1}{k_B} S(E, f_{\text{ex}}, N)}$$

$$\begin{aligned} Z(\beta, f_{\text{ex}}, N) &= \int dE e^{-\beta E + \frac{1}{k_B} S(E, f_{\text{ex}}, N) + o(N)} \\ &= e^{-\beta E_* + \frac{1}{k_B} S(E_*, f_{\text{ex}}, N) + o(N)} \end{aligned}$$

$$\left. \frac{\partial S(E, f_{\text{ex}}, N)}{\partial E} \right|_{E_*} = \beta \quad \Rightarrow \quad E_*(\beta, f_{\text{ex}}, N)$$

# § イントロダクション - 計算

$$\frac{\partial}{\partial \beta} \log Z(\beta, f_{ex}, N) = -E^* - \beta \frac{\partial E^*}{\partial \beta} + \frac{1}{k_B} \left. \frac{\partial S(E, f_{ex}, N)}{\partial E} \right|_{E^*} \frac{\partial E^*}{\partial \beta}$$

$$= -E^*$$

$$\therefore E^* = \langle H \rangle_{\beta, v, N}^c$$

$$S(T, f_{ex}, N) = k_B \log Z(\beta, f_{ex}, N) + \frac{1}{T} \langle H \rangle_{\beta, v, N}^c$$

$$= 2Nk_B \log T + k_B \frac{1}{2} \beta \times f_{ex}$$

$$+ 2Nk_B - \frac{1}{T} \times f_{ex} + \text{const}$$

$$\left\{ \begin{array}{l} \log Z(\beta, f_{ex}, N) = -2N \log \beta + \overbrace{N \log \frac{\sinh(\beta f_{ex})}{\beta f_{ex}}}^{\frac{1}{2} \beta \times f_{ex}} + N C \\ \langle H \rangle_{\beta, f_{ex}, N}^c = 2Nk_B T - x \cdot f_{ex} \end{array} \right.$$

# § イントロビー - 結果 -

$$S(T, f_{ex}, N) = 2N h_B \log T - \frac{1}{2T} \frac{f_{ex}^2}{k_{maw}} + \text{const}$$

10h

270の変位  
の個数  
と 12 が 3.

$$S(T, X, N) = 2N h_B \log T - \frac{k_{maw}}{2T} X^2 + \text{const}$$

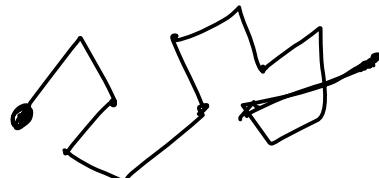
運動量空間  
の 相空間体積の log  
= "状態数" の log  
= 運動の複雑さ

相空間の log  
= 配置の複雑さ

### 現象の角解釈

$$S(T, X, N) = 2N k_B \log T - \frac{K_{\text{マス}}}{2T} X^2 + \text{const}$$

温度  $T$  一定で 变位を与える ( $f_{\text{ex}} \neq 0$ )



- {・自己置の“複雑さ”が減少  
・運動の“複雑さ”が一定
- ・拘束をはずすと、もともと能数  
 $(f_{\text{ex}}=0)$   
が“大き”い能数 ( $X=0$ ) に変化する

復元力！ エントロピー！

~Intermission~

# まとめ

- ▷ 統計力学模型に もとづいて  
エンロピー カ との 復元力  
を 具体的 に 計算 した。
- ▷ エネルギー, エントロピー を 計算 した。  
  
⇒ 来週, この例題の 热力学関係式へ  
( “混ざるする部分 !! ” )